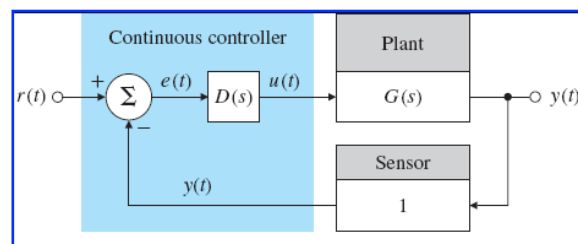


# ME 433 – STATE SPACE CONTROL

## Lecture 7

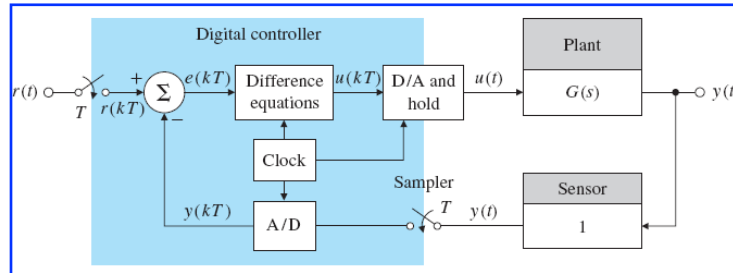
## Time Discretization

### Continuous-time Feedback System



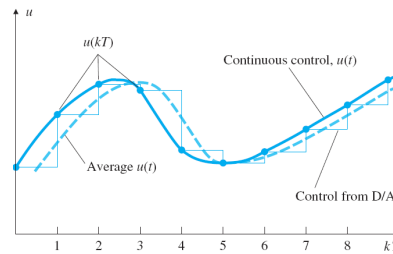
# Time Discretization

## Discrete-time Feedback System



$r(kT), e(kT), u(kT), y(kT)$ : sampled signals

- $T$ : sample period
- $1/T$ : sample rate (Hz)
- A/D: analog-to-digital converter
- D/A: digital-to-analog converter

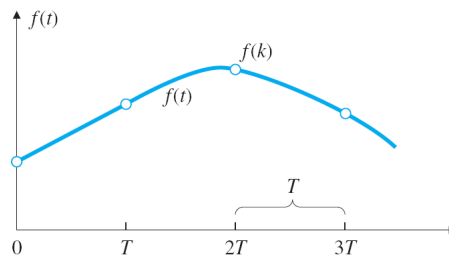


# Time Discretization

## Function $f(kT)$ of time:

$f(k) = f(kT)$  is the sampled version of  $f(t)$ , and  $k=0, 1, 2, 3, \dots$  refer to the discrete sample times  $t_0=0, t_1=T, t_2=2T, t_3=3T, \dots$

$$Z\{f(k)\} = F(z) = \sum_{k=0}^{\infty} f(k)z^{-k}$$



“Differentiation” property:

$$Z\{f(k-1)\} = z^{-1}F(z)$$

## Z-Transform

L-Transform	Waveform	Z-Transform
$\frac{1}{s}$	$1(kT)$	$\frac{z}{z-1}$
$\frac{1}{s^2}$	$kT$	$\frac{Tz}{(z-1)^2}$
$\frac{1}{s+\alpha}$	$e^{-\alpha kT}$	$\frac{z}{z-e^{-\alpha T}}$
$\frac{1}{(s+\alpha)^2}$	$kT e^{-\alpha kT}$	$\frac{Tz e^{-\alpha T}}{(z-e^{-\alpha T})^2}$
$\frac{\beta}{s^2+\beta^2}$	$\sin(\beta kT)$	$\frac{z \sin(\beta T)}{z^2 - 2 \cos(\beta T)z + 1}$
$\frac{s}{s^2+\beta^2}$	$\cos(\beta kT)$	$\frac{z(z - \cos(\beta T))}{z^2 - 2 \cos(\beta T)z + 1}$

## Z-Transform

### Discrete-time System

$$y[k] + a_{k-1}y[k-1] + \dots + a_n y[k-n] = b_o u[k] + \dots + b_m u[k-m]$$

Z Transform

$$(1 + a_1 z + \dots + a_{n-1} z^{n-1} + a_n z^{-n}) Y(z) = (b_o + \dots + b_m z^{-m}) U(z)$$

$$T(z) = \frac{Y(z)}{U(z)} = \frac{b_o + \dots + b_m z^{-m}}{1 + a_1 z + \dots + a_{n-1} z^{n-1} + a_n z^{-n}}$$

# Z-Transform

**Continuous-time System:**

$$f(t) = e^{-\alpha t} \longrightarrow \frac{1}{s + \alpha}$$

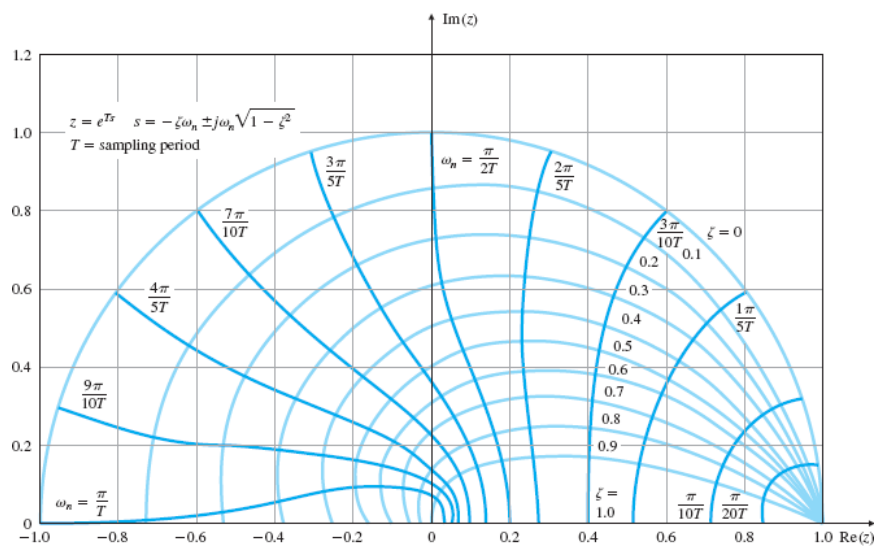
**Discrete-time System:**

$$f(kT) = e^{-\alpha kT} \longrightarrow \frac{z}{z - e^{-\alpha T}}$$

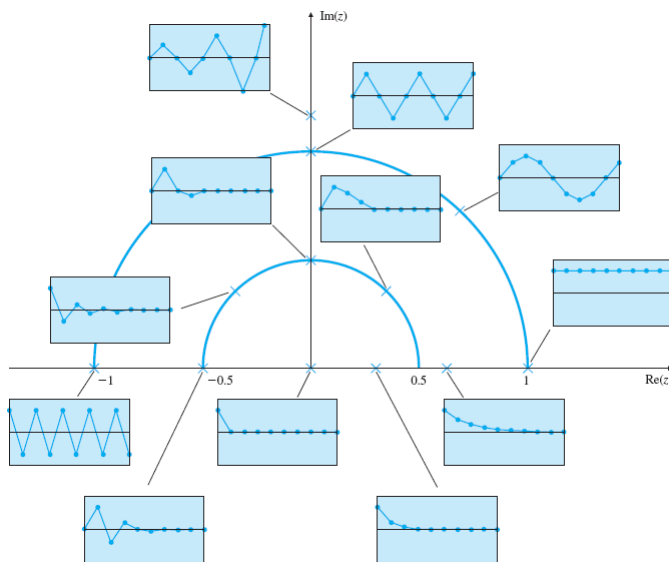
The pole at  $s = -\alpha$  in the s-domain corresponds to a pole at  $z = e^{-\alpha T}$  in the z-domain:

$$z = e^{sT}$$

# Z-Transform

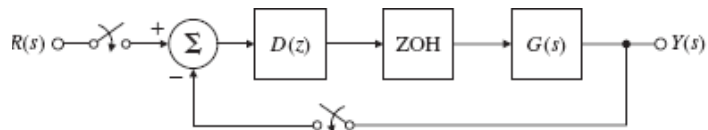


## Z-Transform

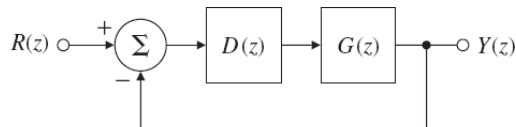


## Control Design

### Emulation (Discrete Equivalent):

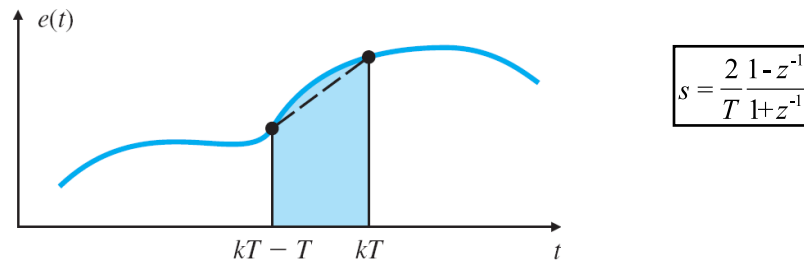
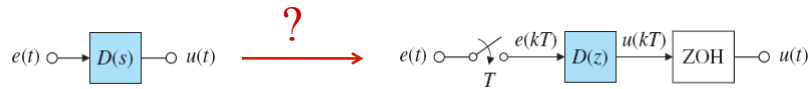


### Discrete Design:



## Discrete Equivalent (Emulation) Design

### Tustin's (Bilinear) Method:



## Discrete Equivalent (Emulation) Design

### Nyquist Theorem:

The Nyquist theorem states that a signal must be sampled at least twice as fast as the bandwidth of the signal to accurately reconstruct the waveform; otherwise, the high-frequency content will *alias* at a frequency inside the spectrum of interest (passband). An alias is a false lower frequency component that appears in sampled data acquired at too low a sampling rate.

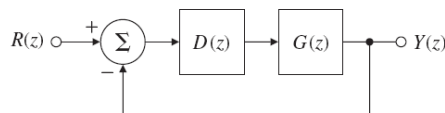
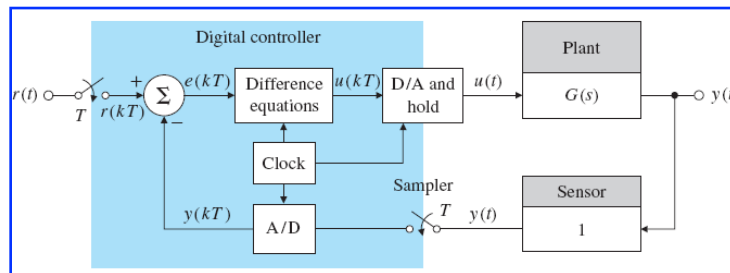
An analog anti-alias filter is often placed between the sensor and the A/D converter. Its function is to reduce the higher-frequency noise components in the analog signal in order to prevent aliasing, that is, having noise or high-frequency components being modulated to a lower frequency by the sampling process.

If designing by discrete equivalents, a minimum sample rate of 20 times the bandwidth is recommended. Typically, even faster sampling is useful for best performance. Computational delay should be less than  $T/10$ .

# Discrete Equivalent (Emulation) Design

Example:

# Discrete Design



What is the TF between  $u(kT)$  and  $y(kT)$ ?

$$G(z) = (1 - z^{-1})Z\{G(s)/s\}$$

## Discrete Design

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Example:

## Solution of State Equation

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We consider the linear, time-invariant system

$$\begin{aligned} \dot{x} &= Ax + Bu, \\ y &= Cx + Du. \end{aligned}$$

The overall solution for the state equation can be written as

$$x(t) = e^{A(t-t_0)} x(t_0) + \int_{t_0}^t e^{A(t-\lambda)} Bu(\lambda) d\lambda$$

and the system output as

$$y(t) = Cx(t) + Du(t) = Ce^{A(t-t_0)} x(t_0) + C \int_{t_0}^t e^{A(t-\lambda)} Bu(\lambda) d\lambda + Du(t)$$



## Solution of State Equation

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Let us now consider  $t_0 = kT$  and  $t = kT + T$ , then

$$x(kT + T) = e^{AT} x(kT) + \int_{kT}^{kT+T} e^{A(kT+T-\lambda)} Bu(\lambda) d\lambda$$

Let us also consider

$$u(t) = u(kT) \quad \forall t \in [kT, kT + T]$$

Using the change of variable  $\eta = kT + T - \lambda$ , we obtain

$$x(kT + T) = e^{AT} x(kT) + \int_0^T e^{A\eta} d\eta Bu(kT)$$

## Solution of State Equation

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Defining

$$\Phi = e^{AT}, \Gamma = \int_0^T e^{A\eta} d\eta B$$

we can write

$$\begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k), \\ y(k) &= Cx(k) + Du(k). \end{aligned}$$

Note that we can write:

$$\Phi = I + AT\Psi$$

$$\Psi = I + \frac{AT}{2!} + \frac{A^2T^2}{3!} + \dots$$

$$\Gamma = \sum_{k=0}^{\infty} \frac{A^k T^{k+1}}{(k+1)!} B = \sum_{k=0}^{\infty} \frac{A^k T^k}{(k+1)!} TB = \Psi TB$$

## Solution of State Equation

---

We consider the linear, time-invariant system

$$\begin{aligned}x(k+1) &= \Phi x(k) + \Gamma u(k), \\y(k) &= Cx(k) + Du(k).\end{aligned}$$

We Z transform the state equation to obtain

$$zX(z) = \Phi X(z) + \Gamma U(z)$$

$$X(z) = Z[x(k)], \quad U(z) = Z[u(k)]$$

And we solve to obtain

$$\frac{Y(z)}{U(z)} = C(zI - \Phi)^{-1}\Gamma + D$$